## ABOVE-GROUND INSTALLATION OF THERMOPLASTIC PIPING

## SUPPORT SPACING OF PLASTIC PIPE

When thermoplastic piping systems are installed aboveground, they must be properly supported to avoid unnecessary stresses and possible sagging.

Horizontal runs require the use of hangers spaced approximately as indicated in tables for individual material shown below. Note that additional support is required as temperatures increase. Continuous support can be accomplished by the use of a smooth structural angle or channel.

Where the pipe is exposed to impact damage, protective shields should be installed.

Tables are based on the maximum deflection of a uniformly loaded, continuously supported beam calculated from:

$$
\mathrm{y}=.00541 \frac{\mathrm{~mL}^{4}}{\mathrm{El}}
$$

Where:
y = Deflection or sag, in.
$\mathrm{w}=$ Weight per unit length, lb./in.
L = Support spacing, in.
$\mathrm{E}=$ Modulus of elasticity at given temp. lb./in. ${ }^{2}$
I = Moment of inertia, in. ${ }^{4}$

If 0.100 in . is chosen arbitrarlly as the permissible sag (y) between supports, then:

$$
\begin{gathered}
\qquad L^{4}=18.48 \frac{\mathrm{El}}{\mathrm{~W}} \\
\mathrm{~W}=\text { Weight of Pipe }+ \text { Weight of Liquid, Ib.in. }
\end{gathered}
$$

$$
e I=\frac{\pi}{64}\left(D o^{4}-D I^{4}\right)
$$

For a plpe $\mathrm{I}=\frac{\pi}{64}\left(\mathrm{Do}^{4}-\mathrm{DI}^{4}\right)$
Where:
Do $=$ Outside diameter of the pipe, in.
$\mathrm{Di}=$ Inside diameter of the pipe, in.
Then:

$$
\left.\mathrm{L}=.907 \frac{E_{W}}{W}\left(\mathrm{Do}^{4}-\mathrm{Di}^{4}\right)^{1 / 4}=.976 \frac{\mathrm{E}_{( }(\mathrm{Do}}{\mathrm{W}}-\mathrm{Di}^{4}\right)^{1 / 4}
$$

Where

Table 1
SUPPORT SPACING"L" (FT) - PYC

|  | NOMINAL PIPE SIZE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F | 12. | $3 / 4$ | 1 | 1-1/4 | t-1d | 2 | 3 | d | 6 | 8 | 10 | 12 |
| SCHEDULE 40 PVC |  |  |  |  |  |  |  |  |  |  |  |  |
| 68 | 4-1: | 4.20 | 5 | S-12 | 5-3. | E-1. | T-10. | 8-3 | 2-102 | 10.12 | 15.14 | 12-10-1 |
| 100 | 4 | 4-21 | 4-3.- | S-1-1 | 5-12. | 6 | 7 | 7-3. | 9 | 10 | 11 | 11.3) |
| 140 | 3.3.4 | 4 | 4-14. | 5 | 5-1. | S-3. | E-24 | r-vi | $8-12$ | 0.34 | 10-v | 11-21 |
| SCHEDULE 80 PVC |  |  |  |  |  |  |  |  |  |  |  |  |
| 62 | 4-12. | 4.2) | 5-1. | 5-34 | c | Q1\% | 3 | 8-3. | 10-1/2 | 11.1.2. | 12.34 | 14 |
| 100 | 4 | 4-10 | 5 | 5-109 | 5.3. | E-1. | 7-12. | B-13- | 10 | 11 | 12.14 | 13-12 |
| 140 | 3-3.4 | 4.14 | 4-3.4 | 5-54 | 5-14 | 5 | 1 | 8 | 2-192 | 30.12. | 12-46 | 12.10 |

Table 2
SUPPORT SPACING "L" (FT.) - CPVC Schedule 80

| $\begin{array}{\|c\|} \hline \text { TEMP } \\ \hline \end{array}$ | NOMINAL PIPE SIZE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 112 | 3.4 | 1 | 1-1/4 | 1-112 | 2 | 3 | 4 | 4 | E | 10 | 12 |
| 73 | 4 | 4-12 | 5 | 5-1/2 | 5-3/4. | Q-1/ | 7.344 | $8.1 / 2$ | 10-284 | 12. 14 | $12-1 / 2$ | 13-3/4 |
| 100 | 4 | 4.12 | 5 | 5-1/2. | 5-3/4. | a-16 | 7-1/2 | $8.1 / 6$ | to | 11 | 12-1/2 | $13-14$ |
| 120 | 4 | 4-1/4 | 4-3/4 | 5-1/4 | 5-1c. | 6-1/0 | 7.12 | 8 81/6 | 9.3.4 | 10-va | 12 | 13 |
| 140 | 4 | 4.14 | 4-3/4 | 5-1/4 | 5-16. | 6 | 7-1/4 | s | 2.12 | 10-12 | 11.3 .4 | 12.344 |
| 560 | 3-34 | 4-114 | 4.1/2 | 5 | 5-1/4 | 5-3.30 | 7 | 7.354 | 2.1.4 | 10-14 | 11-1/2 | 12-16 |
| 180 | 3.345 | 4 | 4-162 | 5 | 5-1/4 | 5-3.09 | 7 | 7-1/2 | - | 10-24 | 11-1/4 | 12.14 |
| 210 | 3 c | 4 | $4 \cdot 124$ | 4-3.30 | 5 | $4-10$ | 6-12 | 7-4/4 | 8.3.4 | 9.3.4 | 100.34 | 11-3/4 |

## ABOVE-GROUND INSTALLATION OF THERMOPLASTIC PIPING

Table 3
SUPPORT SPACING "L" (FT.) - Polypro Schedule 80

| TEMP | NOMINAL PIPE SIZE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 12 | 34 | 1 | 1-1/1/ | $1-18$ | 2 | 3 | 4 | 8 | $\bigcirc$ | 10 | 12 |
| T3 | 3-34 | 4 | 4-8/2 | 4.3/f | 5 | S-v2 | 8, 40 | T-144 | 8.12 | $2 \cdot 1 / 2$ | 50.16 | 13-1 |
| 120 | 3-52 | 3-3M | 4 | 4-16. | 4-3/9 | 5 | 6 | 6-24 | 8 | 8.34 | 2-34 | 10-1 |
| 140 | 3 | 3-16 | 3.34 | 4 | 4-1/4 | 4-1/2 | 5-140 | 8 | 7-1/4 | 8 | 8.34 | a-12 |
| 180 | 3 | 3 | 3-4 | 3.39 | 4 | 4-24- | $5-14$ | $5-34$ | C-3/4 | 7-1/2 | 8.144 | - |
| 150 | 234 | 3 | 3-14. | 3-10 | 3-3/4 | 4 | 5 | 5-120 | \& 12 | 7 | 7-34 | 8-1/2 |
| 200 | 2-52 | 2.34 | 3 | 3-16. | 3-16. | 4 | 4.314 | 5-14 | 8 | 4-3,4 | 7-1/2 | 8 |
| 212 | $2-48$ | 2-3.4 | 3 | 3-114 | 3-1/4 | 3-34 | 4.28 | 5 | 5-344 | 6-1/2 | 7-84 | 7.34 |

Support spacing subject to change with SDR piping systems and different manufacturers' resins. See manufacturers support spacing guide prior to installation.

Table 4
SUPPORT SPACING "L"(FT.) - Proline \& Super Proline

| PIPE SIZE <br> (iN.) | TEMPERATURE |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & 68^{\circ} \mathrm{FI} \\ & 20^{\circ} \mathrm{C} \end{aligned}$ | $\begin{array}{\|l} 86^{\circ} \mathrm{FI} \\ 30^{\circ} \mathrm{C} \end{array}$ | $\begin{aligned} & 104^{\circ} \mathrm{Fl} \\ & 40^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 122^{\circ} \mathrm{Fl} \\ & 50^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 140^{\circ} \mathrm{FI} \\ & 60^{\circ} \mathrm{C} \end{aligned}$ | $\begin{array}{l\|} 158^{\circ} \mathrm{FI} \\ 70^{\circ} \mathrm{C} \end{array}$ | $\begin{aligned} & \hline 176^{\circ} \mathrm{FI} \\ & 80^{\circ} \mathrm{C} \end{aligned}$ |
| 1/2 | 3.0 | 2.5 | 2.5 | 2.0 | 2.0 | 2.0 | 20 |
| 3/4 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 2.5 | 2.0 |
| 1 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 |
| 1-1/2 | 4.0 | 3.5 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| 2 | 4.5 | 4.0 | 4.0 | 3.5 | 3.0 | 3.0 | 3.0 |
| 2-1/2 | 5.0 | 4.5 | 4.0 | 4.0 | 3.5 | 3.0 | 3.0 |
| 3 | 5.5 | 5.0 | 4.0 | 4.0 | 4.0 | 3.5 | 3.5 |
| 4 | 6.0 | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| 6 | 7.0 | 6.0 | 6.0 | 5.0 | 5.0 | 4.5 | 4.5 |
| 8 | 7.5 | 7.0 | 6.0 | 6.0 | 5.5 | 5.0 | 5.0 |
| 10 | 8.5 | 7.5 | 7.0 | 6.5 | 6.0 | 6.0 | 5.5 |
| 12 | 9.5 | 8.5 | 8.0 | 7.0 | 7.0 | 6.5 | 6.0 |
| 14 | 10.0 | 8.5 | 8.0 | 7.5 | 7.0 | 6.5 | 6.5 |
| 16 | 10.5 | 9.5 | 8.5 | 8.0 | 7.5 | 7.0 | 6.5 |
| 18 | 11.5 | 10.0 | 9.0 | 8.5 | 8.0 | 7.5 | 7.0 |
| 20 | 12.0 | 10.5 | 9.5 | 8.5 | 8.5 | 8.0 | 7.5 |
| 24 | 13.5 | 11.5 | 10.0 | 9.5 | 8.5 | 8.0 | 7.5 |

This support spacing chart shows spans for polypropylene (PP) SDR 11, PP SDR 17.6, and PVDF pipes. For PP SDR 32, multiply span times .55 for the reduced value.

The support spacing chart shown above is based on liquids with a specific gravity of 1.0 . Spacing should be reduced by $10 \%$ for liquids having 1.5 specific gravity, $15 \%$ for 2.0 s.q.. and $20 \%$ for 2.5 s.q.

Table 5
SUPPORT SPACING "L" (FT.) - PVDF Schedule 80

|  | NOMINAL PIPE SIZE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\circ}$ | 1/2 | 314 | 1 | 1-14 | 1-1/2 | 2 | 1 | 4 | 5 | 8 | 10 | 12 |
| ds | 3-120 | 3-34 | 4-1/4 | 412 | 4-3/4 | 5-1/4 | 8-1/2 | 7 | 3-1/2 | 0-1/2 | 10-1/2 | 11-1/4 |
| 120 | 3 | 3-14 | $3-34$ | 4 | 4-1/4 | 4-3/4 | 5-3/4 | B-14 | 7-1/2 | B-1/4 | $2 \cdot 14$ | 15 |
| 160 | $2 \cdot 34$ | 3 | 3-1/2 | $3-34$ | 4 | 4-1/4 | 5-1/4 | 5.14 | 6-3.4 | T-N2 | B-120 | 9 |
| 200 | $2 \cdot 12$ | 2-34 | 3 | 3-120 | $3-1 / 2$ | 4 | 4-3/4 | 5-14 | d-1.4 | 7 | 7-144 | B-124 |
| 240 | 2-144 | 2-20 | 2-34 | 3 | 3-1/4 | 3-1/2 | 4-1/4 | 4-14 | 3-1/2 | 6-1/4 | 7 | 7-12 |
| 260 | 2-14 | $2-10$ | 2-344 | 3 | 3-1/4 | $31 / 2$ | 4 | 4-16 | 4-12. | 6 | 8-34 | 7-144 |
| 200 | 2 | $2-14$ | 2.16 | 2.31 | 3 | $3-1 / 4$ | 4 | 414 | 4-14.4 | 5,34 | 6-12 | 7 |

Support spacing subject to change with SDR piping systems and different manufacturers'resins. See manufacturers support spacing guide prior to installation.

NOTE: All tables shown are based in 100 inch SAG between supports.

# BELOW-GROUND INSTALLATION OF THERMOPLASTIC PIPING 

## WIDTH

The width of the trench should be sufficient to provide adequate room for "snaking" the pipe from side to side along the bottom, as described below, and for placing and compacting the side fills. The trench width can be held to a minimum with most pressure piping materials by joining the pipe at the sur-face and then lowering it into the trench after adequate joint strength has been obtained.

## BEDDING

The bottom of the trench should provide a firm, continuous bearing surface along the entire length of the pipe run. It should be relatively smooth and free of rocks. Where hardpan, ledge rock or bounders are present, it is recommended that the trench bottom be cushioned with at least four (4) inches of sand or compacted fine-grained soils.

## SNAKING

To compensate for thermal expansion and contraction, the snaking technique of offsetting the pipe with relation to the trench center line is recommended.

## Example:

Snaking is particularly Important when laying small diameter pipe in hot weather. For example, a 100-foot length of PVC Type I pipe will expand or contract about $3 / 4$ " for each $20^{\circ} \mathrm{F}$ temperature change. On a hot summer day, the direct rays of the sun on the pipe can drive the surface temperature up to $150^{\circ} \mathrm{F}$. At night, the air temperature may drop to $70^{\circ} \mathrm{F}$. In this hypothetical case, the pipe would undergo a temperature change of $80^{\circ} \mathrm{F}$-and every 100 feet of pipe would contract $3^{\prime \prime}$. This degree of contraction would put such a strain on newly cemented pipe joints that a poorly made joint might pull apart.

## Installation:

A practical and economical method is to cement the line together at the side of the trench during the normal working day. When the newly cemented joints have dried, the pipe is snaked from one side of the trench to the other in gentle alternate curves. This added length will compensate for any con-traction after the trench is backfilled. See Figure 1.

Figure 1
The illustration shown below gives the required loop length, in feet, and offset in inches, for various temperature variations.
Snaking of Pipe Within Trench.


Snaking of thermoplastic pipe within trench to compensate for thermal expansion and contraction.

Table 1
SNAKING LENGTH VS. OFFSET (IN.) TO COMPENSATE FOR THERMAL CONTRACTION

| smaking LENGTH (FT.) | MAXIMUM TEMPERATURE VARIATION ("F) BETWEEN TIME OF CEMENTING AND FINAL BACKFFLLING |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $10^{*}$ | $20^{*}$ | $30^{*}$ | $40^{\circ}$ | $50^{\circ}$ | $60^{\circ}$ | $70^{*}$ | $80^{*}$ | $90^{\circ}$ | $100^{\circ}$ |
|  | LOOP OFFSET (IN.) |  |  |  |  |  |  |  |  |  |
| 20 | 2.5 | 3.5 | 4.5 | 5.20 | 5.75 | 6.25 | 6.75 | 7.25 | 7.75 | 8.00 |
| 50 | 6.5 | 9.0 | 11.0 | 12.75 | 14.25 | 15.50 | 17.00 | 18.00 | 19.25 | 20.25 |
| 100 | 13.0 | 18.0 | 22.0 | 26.00 | 29.00 | 31.50 | 35.00 | 37.00 | 40.00 | 42.08 |

DETERMINING SOIL LOADING FOR FLEXIBLE PLASTIC PIPE, SCHEDULE 80
Underground pipes are subjected to external loads caused by the weight of the backfill material and by loads applied at the surface of the fill. These can range from static to dynamic loads.
Static loads comprise the weight of the soil above the top of the pipe plus any additional material that might be stacked above ground. An important point is that the load on a flexible pipe will be less than on a rigid pipe buried in the same manner. This is because the flexible conduit transfers part of the load to the surrounding soil and not the reverse. Soil loads are minimal with narrow trenches until a pipe depth of 10 feet is attained.
Dynamic loads are loads due to moving vehicles such as trucks, trains and other heavy equipment. For shallow burial conditions live loads should be considered and added to static loads, but at depths greater than 10 feet, live loads have very little effect.
Soil load and pipe resistance for other thermoplastic piping products can be calculated using the following formula.
$W c^{\prime}=\frac{\Delta x\left(E I+.06 I E^{\prime} r^{3}\right) 80}{r^{3}}$
Wc' = Load Resistance of the Pipe, lb./ft.
$\Delta x=$ Deflection in Inches @ $5 \%$ ( $05 \times$ I.D.)
$\mathrm{E}=$ Modulus of Elasticity
$\mathrm{t}=$ Pipe Wall Thickness, in.
$r=$ Mean Radius of Pipe (O.D. - t)/2
$\mathrm{E}^{\prime}=$ Modulus of Passive Soil Resistance, psi
$\mathrm{H}=$ Height of Fill Above Top of Pipe, ft.
$I=$ Moment of Inertia $t^{3}$
12
Table 2
LIVE LOAD FOR BURIED FLEXIBLE PIPE (LBJLIN.FT)

| PIPE <br> SIZE | H20 WHEEL LOADS FOR VARIOUS |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 4 | 6 | 8 | 10 |
|  | 309 | 82 | 38 | 18 | 16 |
| 3 | 442 | 118 | 56 | 32 | 21 |
| 4 | 574 | 154 | 72 | 42 | 27 |
| 6 | 837 | 224 | 106 | 61 | 40 |
| 8 | 1102 | 298 | 141 | 82 | 53 |
| 10 | 1361 | 371 | 176 | 101 | 66 |
| 12 | 1601 | 440 | 210 | 120 | 78 |

NOTE H20 wheel losed is $16,000 \mathrm{lb}$ haheel

## BELOW-GROUND INSTALLATION OF THERMOPLASTIC PIPING

Table 3
SOIL LOAD AND PIPE RESISTANCE FOR
FLEXIBLE THERMOPLASTIC PIPE
PVC Schedule 40 and 80 Pipe

| NOM.SIZE(N.) | $\begin{gathered} \text { Wc' = LOAD RESISTANCE OF } \\ \text { PIPE (LB./FT.) } \end{gathered}$ |  |  |  | $\left\lvert\, \begin{gathered} \mathrm{H} \\ (\mathrm{FT}) \end{gathered}\right.$ | Wc = SOIL LOADS AT VARIOUS TRENCH WIDTHS AT TOP OF PIPE (LBJFT.) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SCHEDULE 40PIPE |  | $\begin{gathered} \text { SCHEDULE } 80 \\ \text { PIPE } \\ \hline \end{gathered}$ |  |  |  |  |  |  |
|  | $E^{\prime}=200$ | $E^{\prime}=700$ | $E^{\prime}=200$ | $\mathrm{E}^{\prime}=700$ |  | 2 FT | 3 FT | 4 FT | 5 FT |
| 1-1/2 | 1094 | 12 E 2 | 2908 | 2993 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\begin{gathered} 106 \\ 138 \\ 144 \\ - \end{gathered}$ | $\begin{aligned} & 125 \\ & 182 \\ & 207 \\ & 214 \end{aligned}$ | $\begin{aligned} & 136 \\ & 212 \\ & 254 \\ & 268 \end{aligned}$ | $\begin{array}{\|l\|l} 152 \\ 233 \\ 314 \\ 318 \end{array}$ |
| 2 | 879 | 1130 | 2344 | 2581 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\begin{gathered} 132 \\ 172 \\ 180 \\ - \end{gathered}$ | $\begin{aligned} & 156 \\ & 227 \\ & 259 \\ & 257 \end{aligned}$ | $\begin{aligned} & 170 \\ & 255 \\ & 317 \\ & 337 \end{aligned}$ | $\begin{aligned} & 190 \\ & 291 \\ & 392 \\ & 398 \end{aligned}$ |
| 2-1/2 | 1344 | 1647 | 3218 | 3502 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\begin{gathered} 160 \\ 204 \\ 216 \\ - \end{gathered}$ | $\begin{aligned} & 191 \\ & 273 \\ & 305 \\ & 323 \end{aligned}$ | $\begin{aligned} & 210 \\ & 321 \\ & 377 \\ & 408 \end{aligned}$ | $\begin{aligned} & 230 \\ & 362 \\ & 474 \\ & 482 \end{aligned}$ |
| 3 | 1126 | 1500 | 2818 | 3173 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\begin{gathered} 156 \\ 256 \\ 266 \\ - \end{gathered}$ | $\begin{aligned} & 231 \\ & 335 \\ & 265 \\ & 394 \end{aligned}$ | $\begin{aligned} & 252 \\ & 392 \\ & 394 \\ & 497 \end{aligned}$ | $\begin{aligned} & 290 \\ & 429 \\ & 459 \\ & 596 \end{aligned}$ |
| 3-1/2 | 1021 | 1453 | 2591 | 3002 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\left\|\begin{array}{c} 223 \\ 284 \\ 300 \\ - \end{array}\right\|$ | $\begin{aligned} & 256 \\ & 380 \\ & 425 \\ & 450 \end{aligned}$ | $\begin{aligned} & 293 \\ & 446 \\ & 524 \\ & 568 \end{aligned}$ | $\begin{aligned} & 320 \\ & 490 \\ & 660 \\ & 670 \end{aligned}$ |
| 4 | 909 | 1459 | 2456 | 2922 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\begin{aligned} & 252 \\ & 328 \\ & 342 \end{aligned}$ | $\begin{aligned} & 297 \\ & 432 \\ & 493 \\ & 505 \\ & \hline \end{aligned}$ | $\begin{aligned} & 324 \\ & 540 \\ & 603 \\ & 639 \end{aligned}$ | $\begin{aligned} & 360 \\ & 561 \\ & 743 \\ & 754 \end{aligned}$ |
| 5 | 895 | 1511 | 2272 | 2851 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\begin{aligned} & 310 \\ & 395 \\ & 417 \\ & - \end{aligned}$ | $\begin{aligned} & 370 \\ & 529 \\ & 592 \\ & 625 \end{aligned}$ | $\begin{aligned} & 407 \\ & 621 \\ & 730 \\ & 750 \end{aligned}$ | 445 <br> 681 <br> 918 <br> 932 |
| 6 | 880 | 1620 | 2468 | 3173 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\left(\left.\begin{array}{l} 371 \\ 484 \\ 503 \\ - \end{array} \right\rvert\,\right.$ | $\begin{aligned} & 437 \\ & 630 \\ & 725 \\ & 745 \end{aligned}$ | $\begin{aligned} & 477 \\ & 742 \\ & 898 \\ & 341 \\ & \hline \end{aligned}$ | $\begin{array}{\|c} 530 \\ 812 \\ 1093 \\ 11110 \end{array}$ |
| 8 | 911 | 1885 | 2350 | 3290 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\left\|\begin{array}{c} 483 \\ 630 \\ 656 \\ - \end{array}\right\|$ | 569 <br> 828 <br> 345 <br> 370 | $\begin{array}{\|c} 621 \\ 966 \\ 11150 \\ 1225 \end{array}$ | $\begin{array}{\|l\|} 600 \\ 1067 \\ 1422 \\ 1422 \\ 1445 \end{array}$ |
| 10 | 976 | 2198 | 2597 | 3764 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\left(\left.\begin{array}{c} 602 \\ 785 \\ 817 \\ - \end{array} \right\rvert\,\right.$ | $\begin{gathered} 710 \\ 1092 \\ 1177 \\ 1209 \end{gathered}$ | $\left\lvert\, \begin{gathered} 774 \\ 1204 \\ 1405 \\ 1527 \end{gathered}\right.$ | $\begin{gathered} 860 \\ 1317 \\ 1374 \\ 1801 \end{gathered}$ |
| 12 | 1058 | 2515 | 2909 | 4298 | $\begin{aligned} & 10 \\ & 20 \\ & 30 \\ & 40 \end{aligned}$ | $\begin{aligned} & 714 \\ & 931 \\ & 909 \\ & - \end{aligned}$ | $\begin{gathered} 942 \\ 1225 \\ 1307 \\ 1434 \end{gathered}$ | $\begin{array}{\|c\|} 919 \\ 1429 \\ 1709 \\ 1811 \end{array}$ | $\left\lvert\, \begin{aligned} & 1020 \\ & 1562 \\ & 2104 \\ & 2135 \end{aligned}\right.$ |

NOTE 1: Figures are calculated from minimum soil resistance values ( $\mathrm{E}^{\prime}=200$ psi for uncompacted sandy clay loam) and compacted soil ( $E^{\prime}=700$ for side-fill that is compacted to $90 \%$ or more of Proctor
Density for distance of two pipe diameters on each side of the pipe). If Wc' is less than Wc at a given trench depth and width, then soil compaction will be necessary.


Note: $\mathrm{H}=$ Height of fill above top of pipe, ft. $\mathrm{W}=$ Trench width at top of pipe, ft.

## HEAVY TRAFFIC

When plastic pipe is installed beneath streets, railroads, or other surfaces that are subjected to heavy traffic and resulting shock and vibration, it should be run within a protective metal or concrete casing.

NOTE 2: These are soil loads only and do not include live loads.

